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# Multilayer Coatings for Constellation-X

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## Approach:

- **Replace the baseline iridium SXT mirror coatings with multilayers**

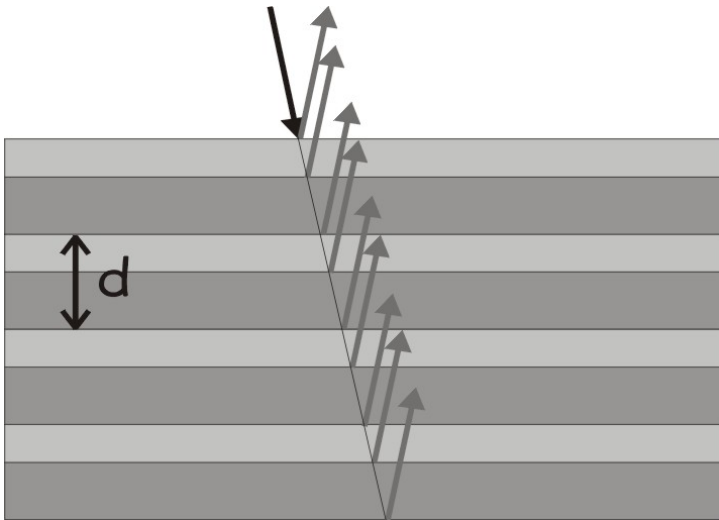
## Benefits:

- *Enhanced throughput over the nominal 0.3 – 10 keV bandpass*
- *Extended response to 40 keV*

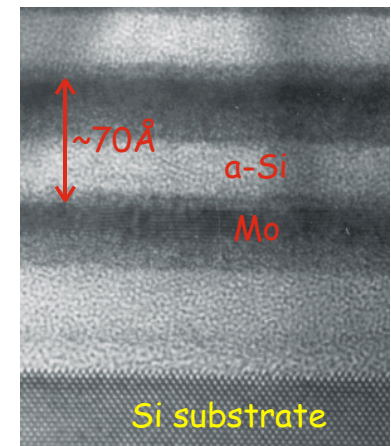
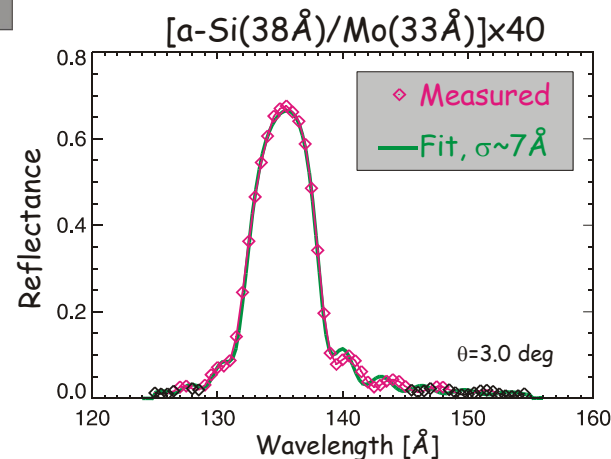
## Costs:

- *Not so much...*

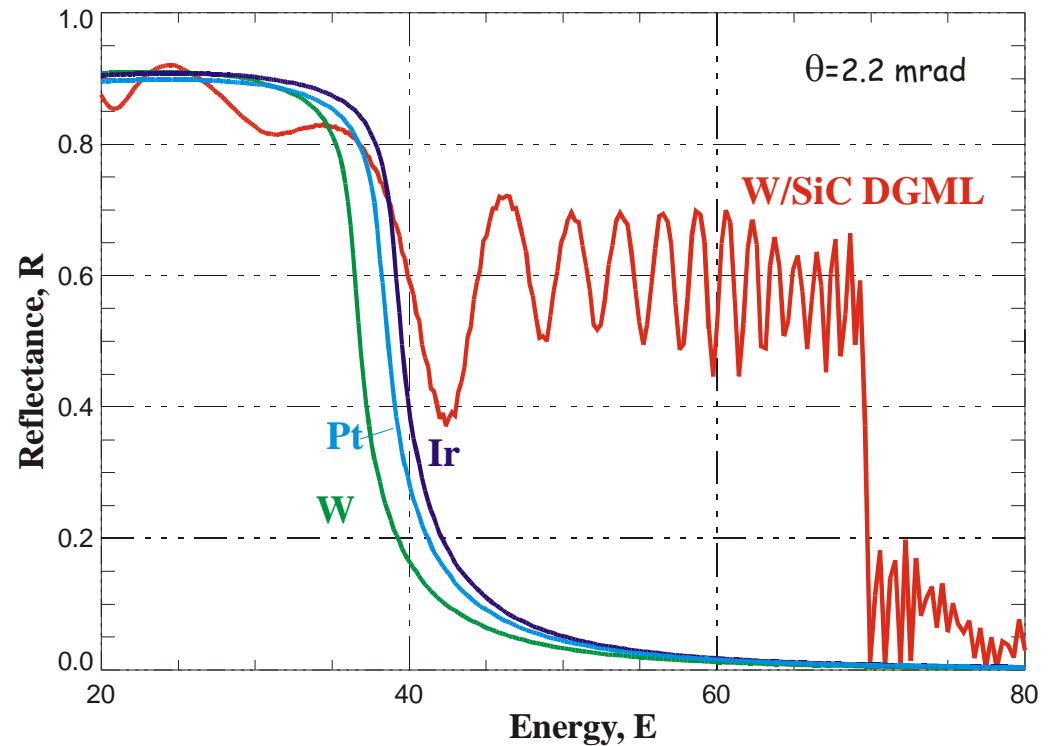
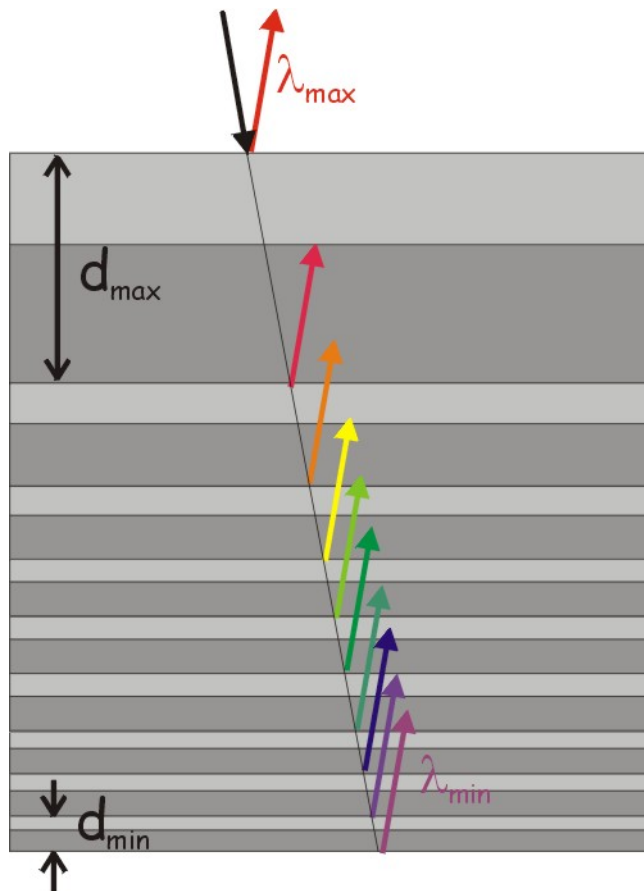
**Periodic Multilayers:** use constructive interference between reflections from each interface in the layer stack to provide high reflectance, as per Bragg's law ( $n\lambda=2d \sin\theta$ )

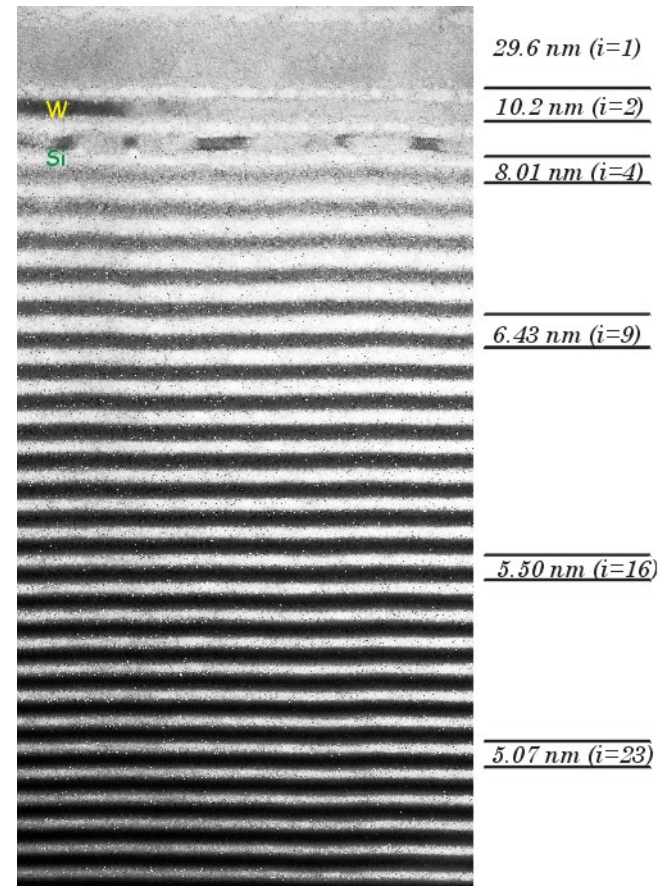
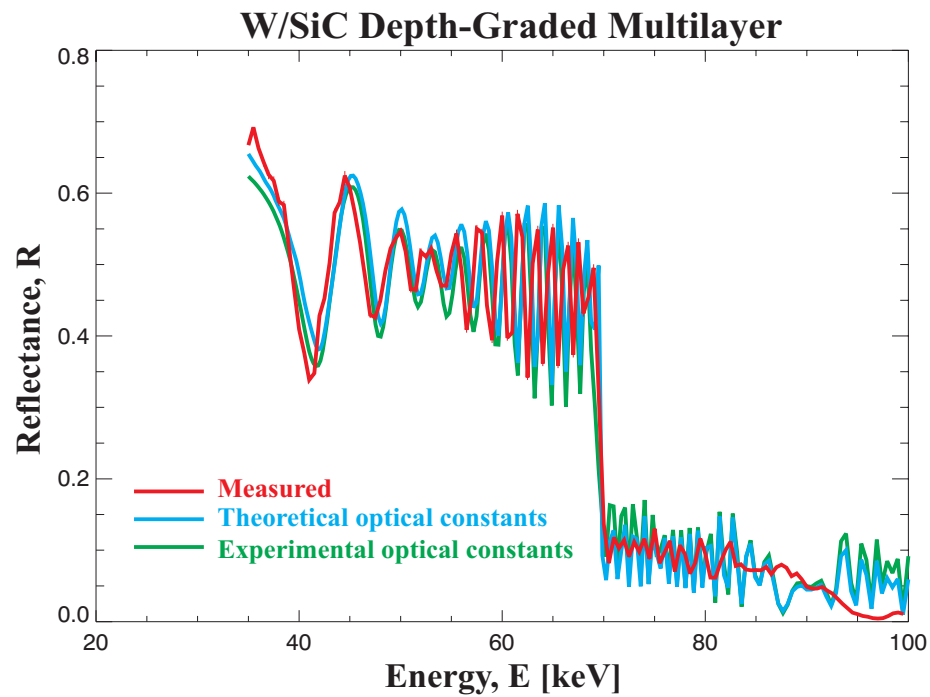


The Bragg condition is satisfied only over a narrow range of angles and wavelengths (energies).



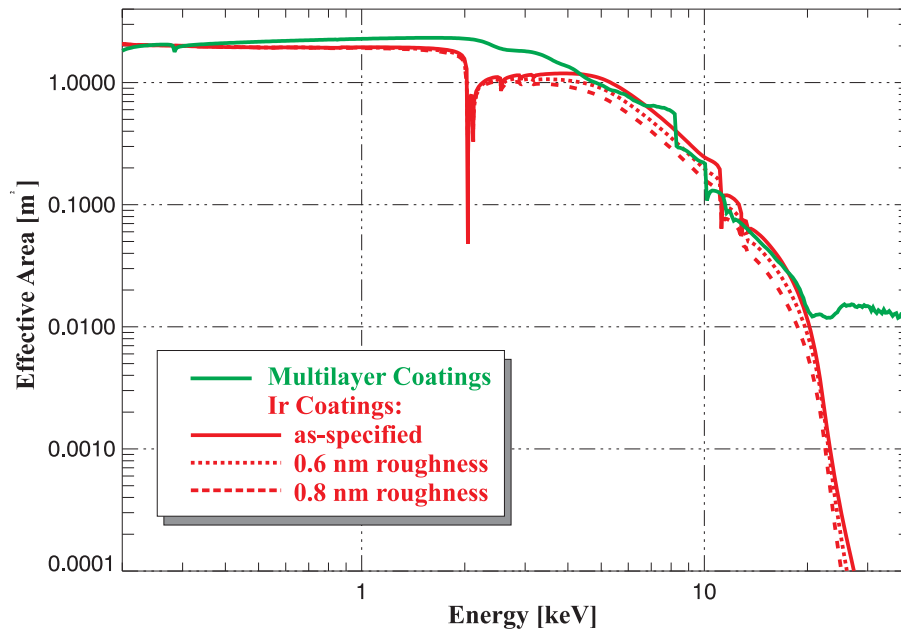
**Depth-Graded Multilayers (DGML):** by growing a film with a range of periods, broad energy response can be achieved.





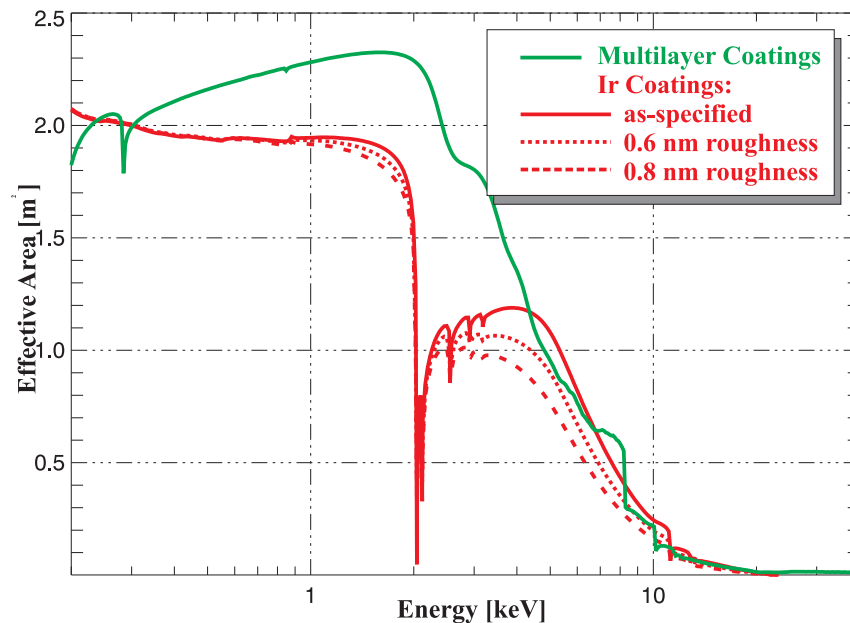
## Multilayer design approach used for the Con-X SEP:

- ‘conventional’ power-law DGML recipe
  - material combinations, layer thicknesses and interface parameters that are realistic, i.e., can be made using current deposition technology
  - DGML recipe customized (albeit ‘manually’) for each of the 163 SXT mirror shells, with graze angles in the range  $0.217^\circ - 0.937^\circ$
- ✍ resulting preliminary design is thus practical, but not necessarily optimal!

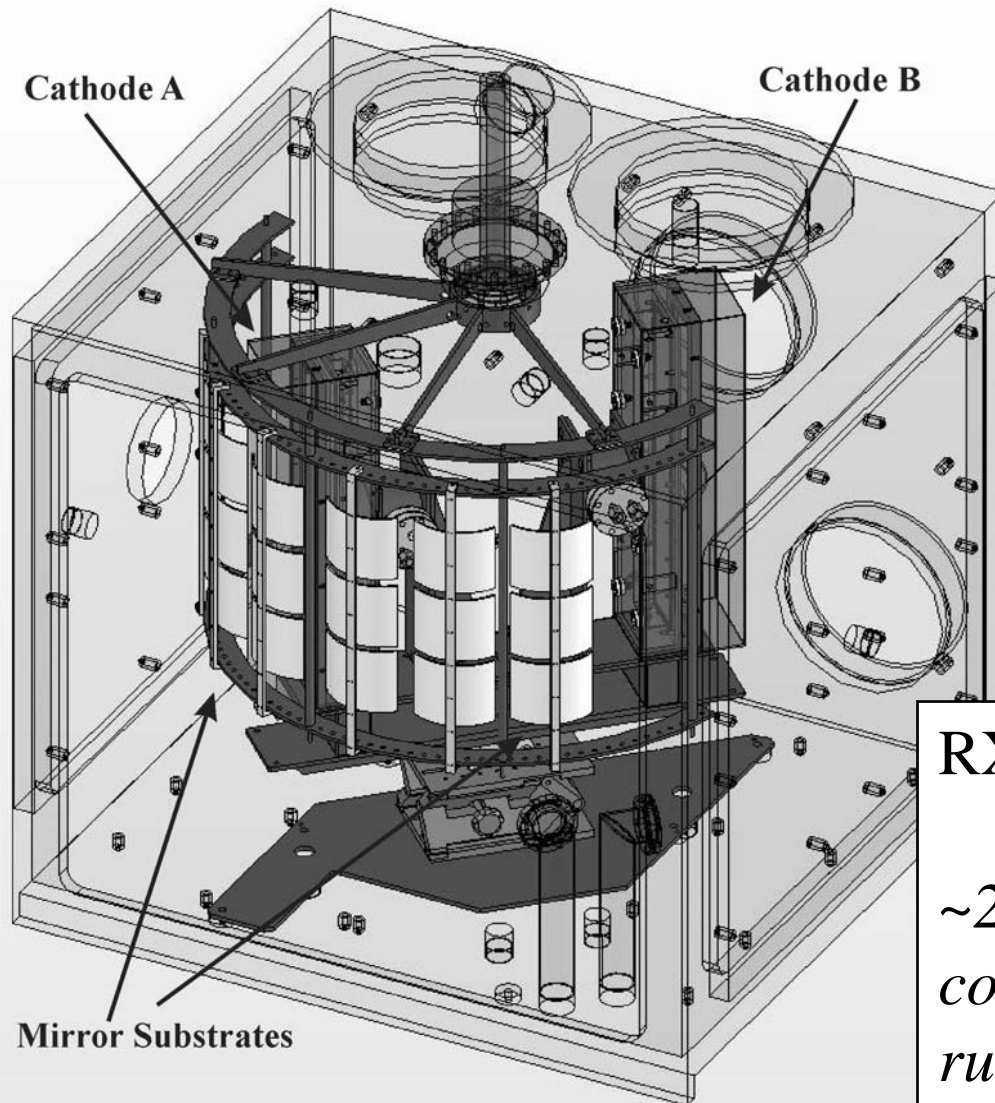


- Significant increase in effective area from ~0.3 keV – ~4.5 keV.

- ~100 – 200 sq. cm. effective area from ~20 – 40 keV.







RXO's coating facility

*~2,500 sq. cm. area can be coated per run, with 1 – 2 runs per day.*



## 1. Estimation of DGML stress on the optical figure, and comparison relative to Ir coatings?

Relationship between film stress,  $\sigma$ , and substrate deformation, i.e., change in radius of curvature (Stoney's equation):

$$\sigma = \frac{Y_s}{6} \frac{t_s^2}{t_f} \left( \frac{1}{R} - \frac{1}{R_0} \right)$$

where  $Y_s$ =substrate biaxial elastic modulus (~92 GPa for glass),  $t_f$ =film thickness,  $t_s$ =substrate thickness, and  $R$  is the substrate radius of curvature.

Don't yet know what the multilayer stress will be, but worst case should be  $\sigma=1$  GPa. Taking  $t_s=400$   $\mu\text{m}$ ,  $t_f=2$   $\mu\text{m}$ ,  $R_0=355$  mm, this gives  $R=275$  mm. (In actuality it should be much less than this.)

In comparison, for a 50-nm-thick Ir film w/  $\sigma=300$  Mpa,  $R=354$  mm.

In any case, once the change in radius is known and predictable it can be accommodated by fabricating the mirror shells such that the final radius  $R$ , rather than the initial radius  $R_0$ , has the required value.

## 2. Impact of surface roughness?

Surface roughness will degrade the reflectance of multilayer-coated mirrors just as it degrades front-surface (i.e., Ir-coated) mirrors.

But: new multilayer technology currently under development may be able to smooth surface roughness intrinsic to the glass.

## 3. Cost?

Pretty hard to say at this point, but perhaps about \$5M, within a factor of 2.

## 4. What about increase from 10 – 20 keV?

Have not yet been able to increase the telescope response in this energy range.

But: the preliminary design shown here is far from comprehensive. Better multilayer designs may be found that do improve the response from 10 – 20 keV.